



Design the Future e-Mobility

Altair HyperWorks Electromechanical Workflow
for the Design of Electric Motor Powertrain

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Richard Yen, SVP, Global Automotive and Industry Verticals Team

April 11 2019



AGENDA

- 1 E-Mobility Trends and Challenges**
- 2 Altair's Vision and Workflow**
- 3 E-Motor Design Process**
- 4 Looking Forward**



MOBILITY TRENDS AND CHALLENGES

Richard Y.



Today's Products are Complex

Connected & Automated



..... E-MOBILITY

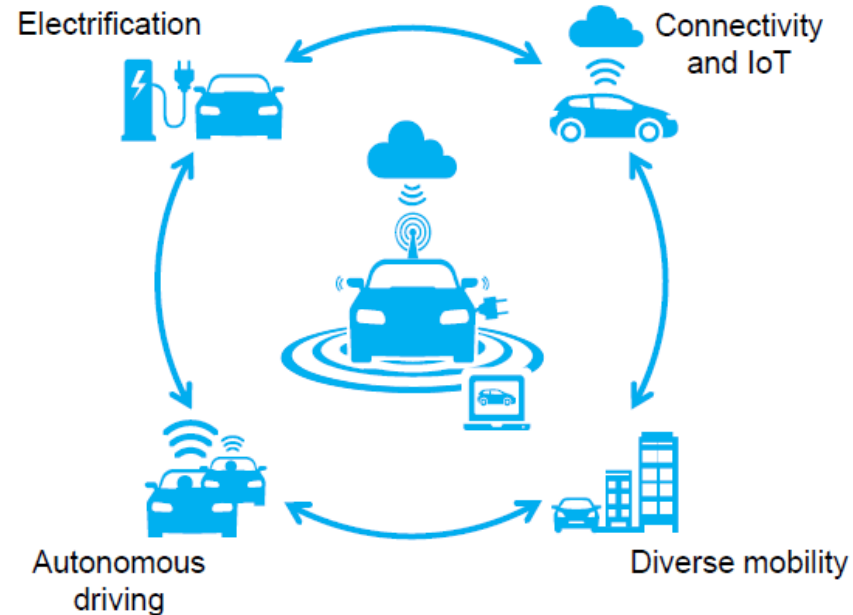
Transportation OEM need sustainable technologies to meet customer demands:
**Safer, Lighter, Greener,
Smarter** Vehicles



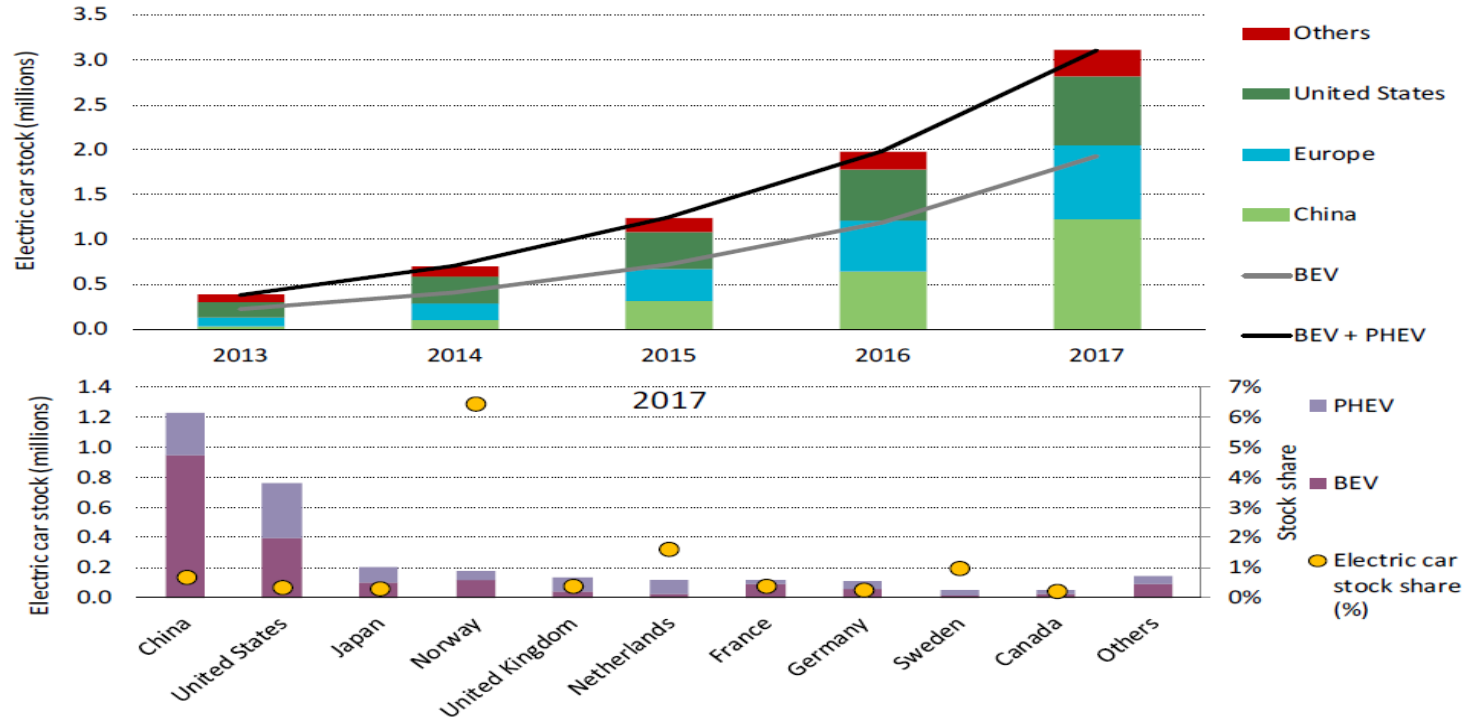
“GM’s vision is a world with zero crashes, zero emissions and zero congestion.”

“GM believes the future of personal mobility will be driven by the convergence of electrification, autonomous vehicles, connectivity and shared mobility services.”

--Mary Barra, CEO of General Motors



INDUSTRY TRENDS ON ELECTRIFICATION (1)

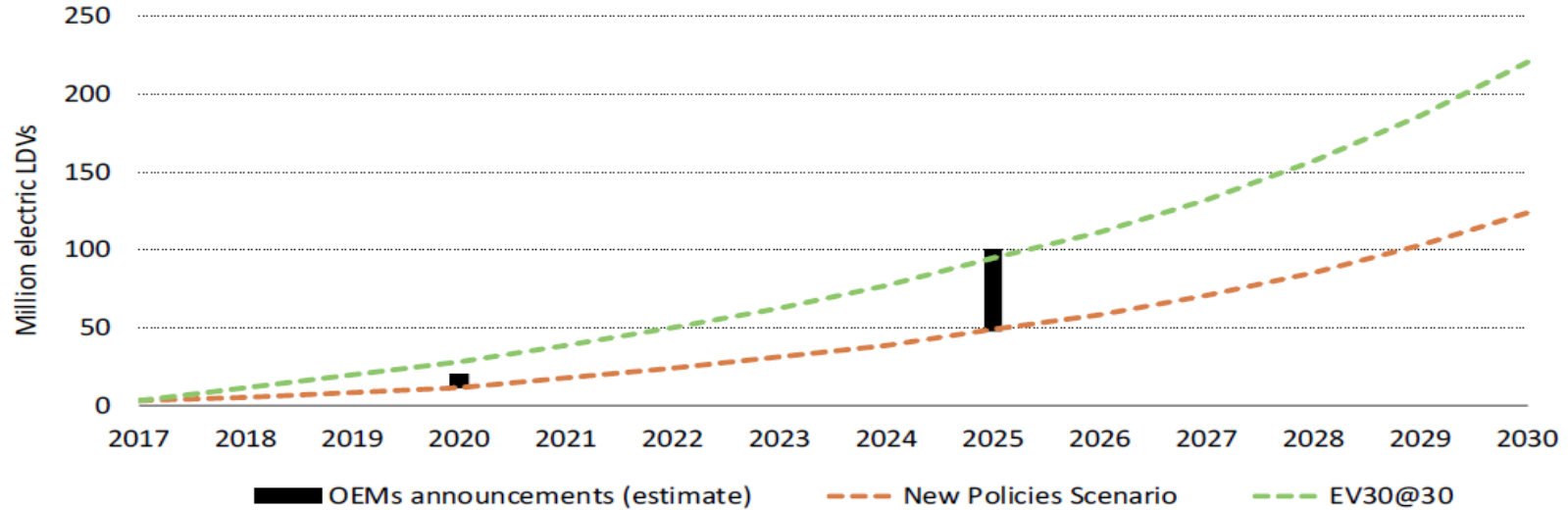


Note: BEV = battery electric vehicle; PHEV = plug-in hybrid electric vehicle. Stock shares are calculated based on country submissions and estimates of the rolling vehicle stocks developed for the IEA Mobility Model. The vehicle stocks are estimated based on new vehicle registration data, lifetime range of 13-18 years, and vehicle scrappage using a survival curve that declines linearly in the last five years of the active vehicle life. Lifetimes at the low end of the range are used for countries with higher income levels (and vice versa).

Source: IEA analysis based on country submissions, complemented ACEA (2018), EAFO (2018a).



INDUSTRY TRENDS ON ELECTRIFICATION (2)



Notes: The 2020 and 2025 projections from original equipment manufacturers are based on their announcements as outlined in Table 2.5. The production capacity of OEMs in China has been capped at 5.2 million vehicles both in 2020 and 2025. This cap is calculated considering the 7.7 million vehicle capacity announced for 2020 (Liu, 2018) and a 66% capacity utilisation factor, aligned with the ratio of vehicle production in China and capacity available in recent years (IHS Markit, 2015). The lower bound of vehicle production in China for 2020 was assumed to be 2 million, well below the capacity assessed to become available in the same year. For companies that announced the deployment of a number of models, the assumptions made in this analysis consider a sales-to-model ratio range of 10 000-30 000 in the 2020 timeframe and 30 000-50 000 in 2025.

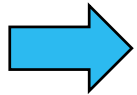
Source: IEA analysis developed with the IEA Mobility Model (IEA, 2018a).

Comparison of scenario projections and manufacturers' targets for electric LDVs, 2017-30



AUTOMOTIVE – ALTAIR'S STRATEGIC SOLUTIONS

- 1 **e-Mobility**
- 2 **Connected and Automated Mobility**
- 3 **Design for Efficiency**
- 4 **Safety, Comfort and Perceived Quality**



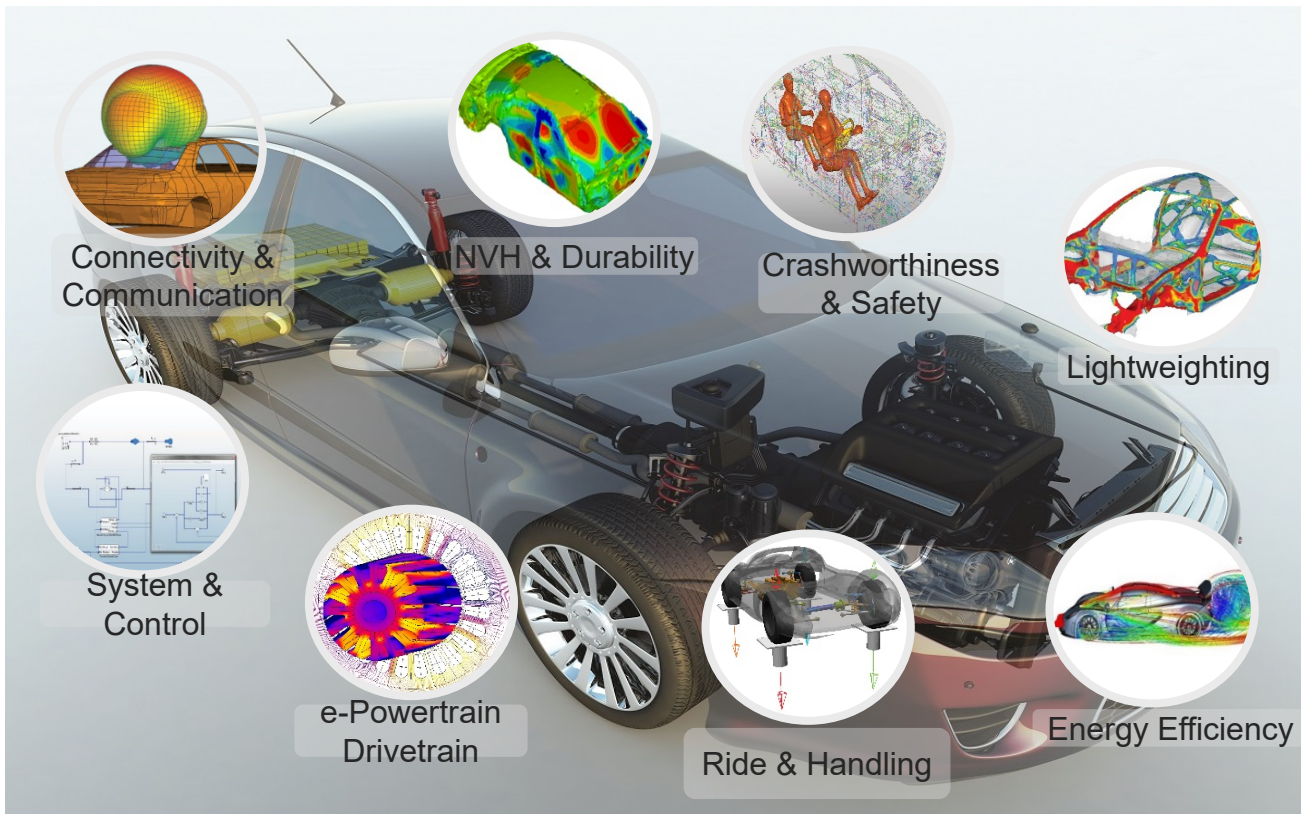
Solution Oriented Innovation

Industry domain knowledge + Integrated design process + Optimization

Design the Difference



DESIGN THE FUTURE OF E-MOBILITY



New Key Elements

- Electric Motor
- Battery
- Power Electronics - Inverter
- System Modeling and Control

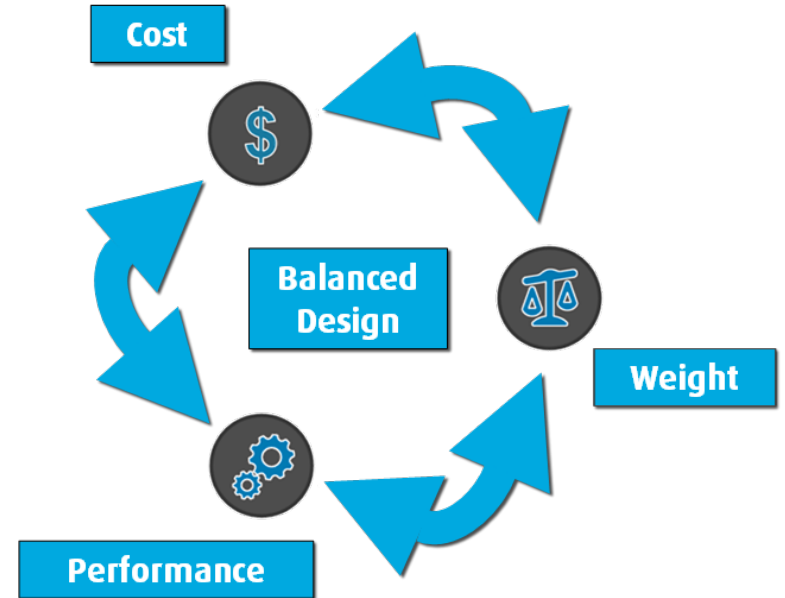
Challenges:

- Packaging and Weight Distribution
- New Requirements and Physics
- Complex System



CHALLENGES FOR E-PROPULSION DESIGN

- **Stringent performance requirements** – Advanced OEMs are trying to set them apart from competition
- **Stricter regulations (WLTP)** – Maximize efficiency throughout the e-propulsion system
- **Multiphysics** design to balance **cost, time, size, weight and performance**
- **Integrated solution** across departments with different disciplinary requirements

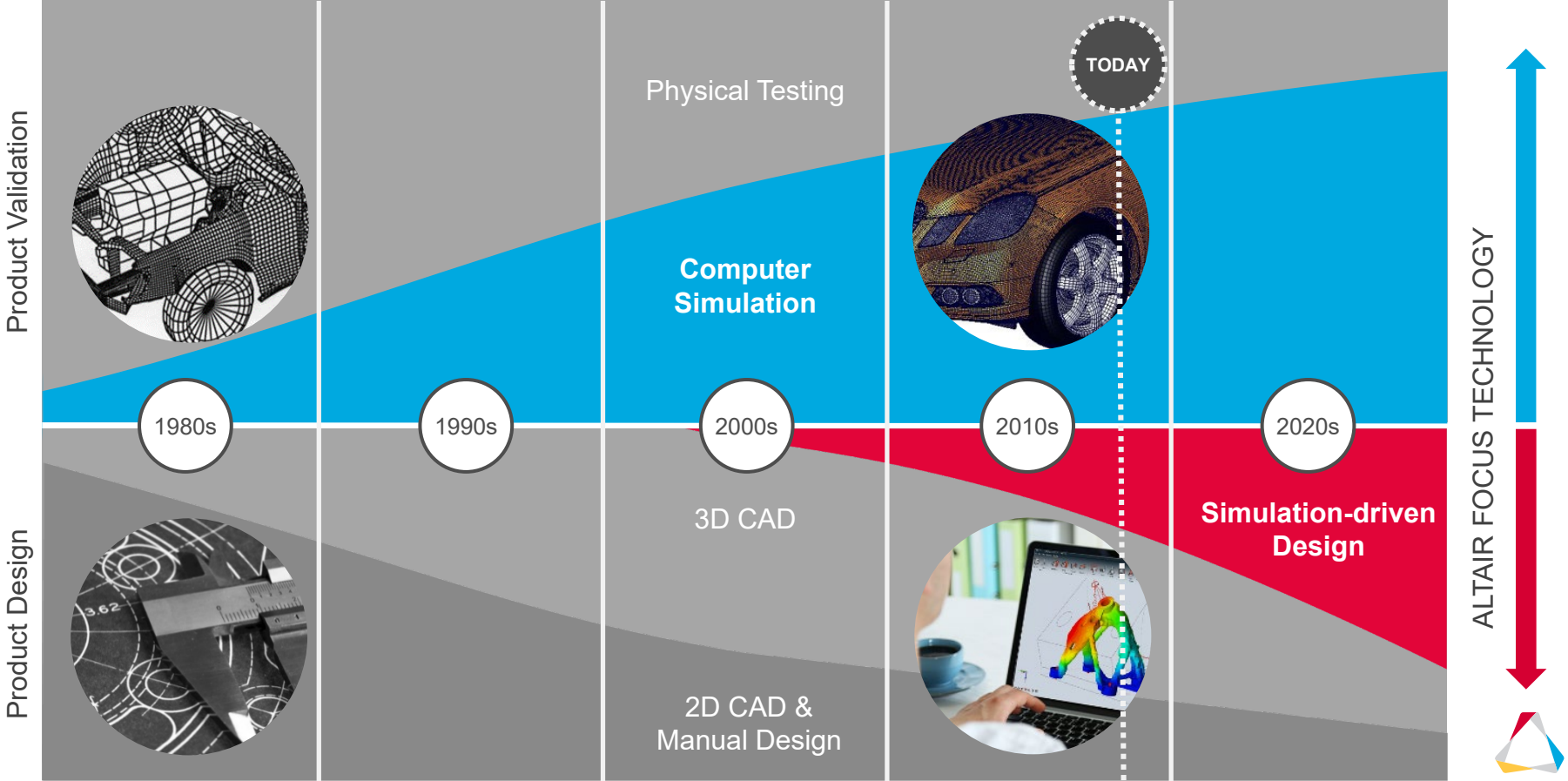


ALTAIR'S VISION AND WORKFLOW

Richard Y.

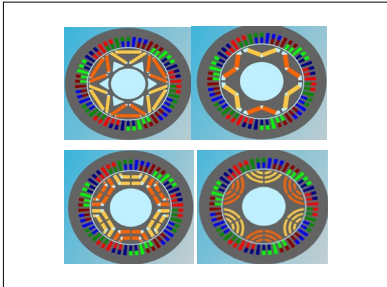


SIMULATION-DRIVEN DESIGN – AN OVERVIEW

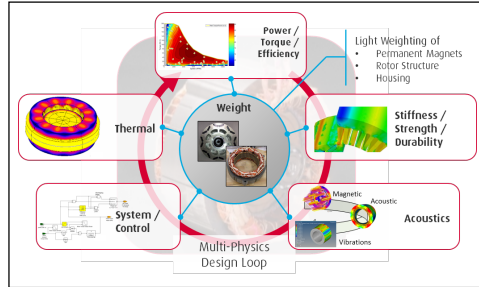


SIMULATION-DRIVEN INNOVATION

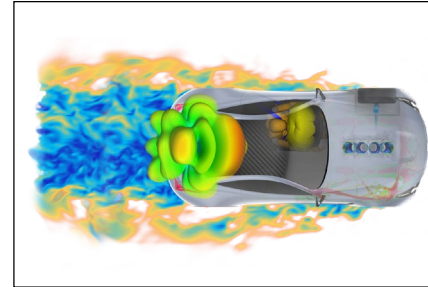
Exhaustive Design Exploration



Optimization & Multiphysics



Powerful Modeling & Visualization



Cloud Collaboration & Data Analytics



High Performance Computing

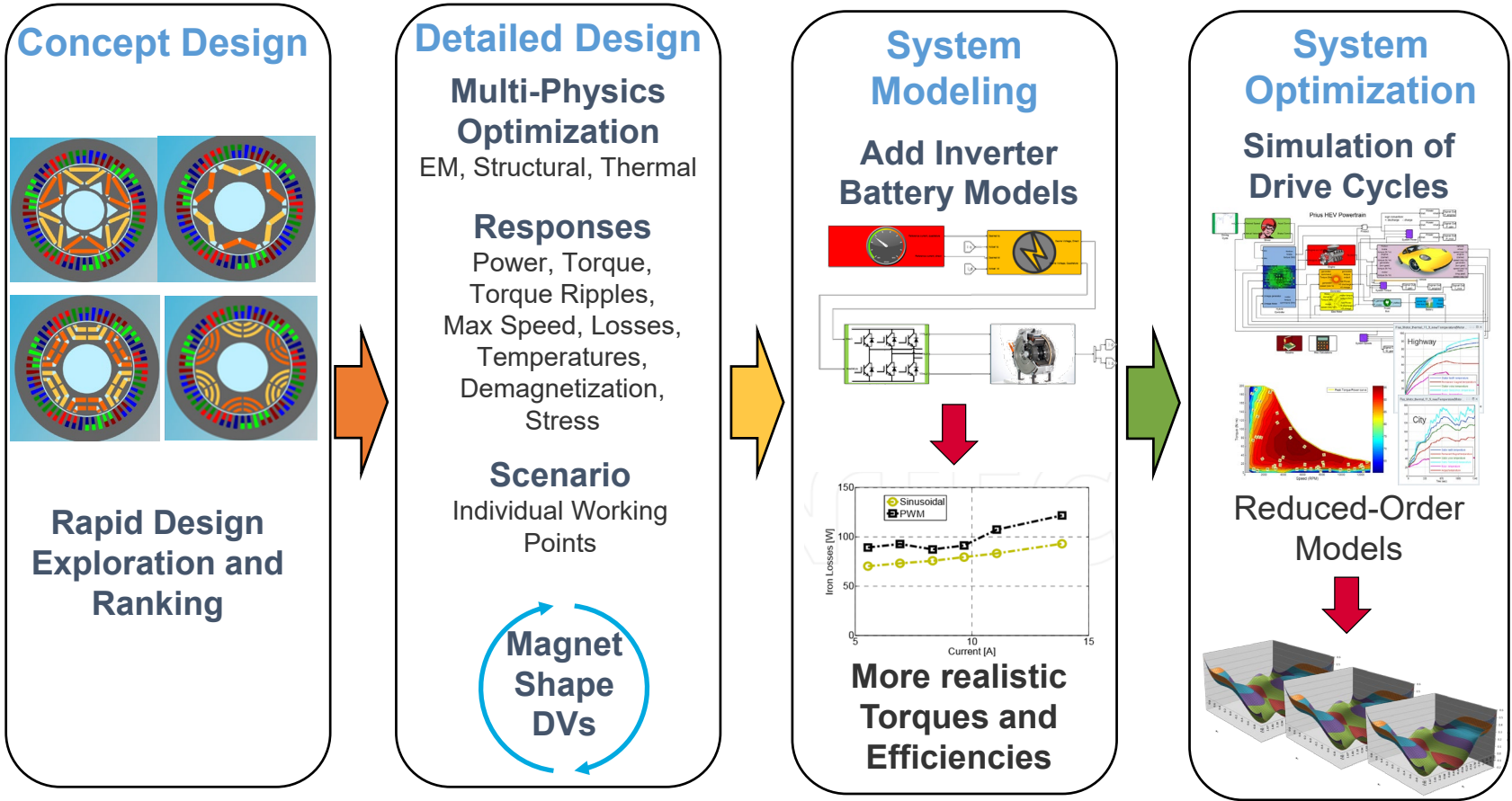


Value-based Business Model

Global Expertise

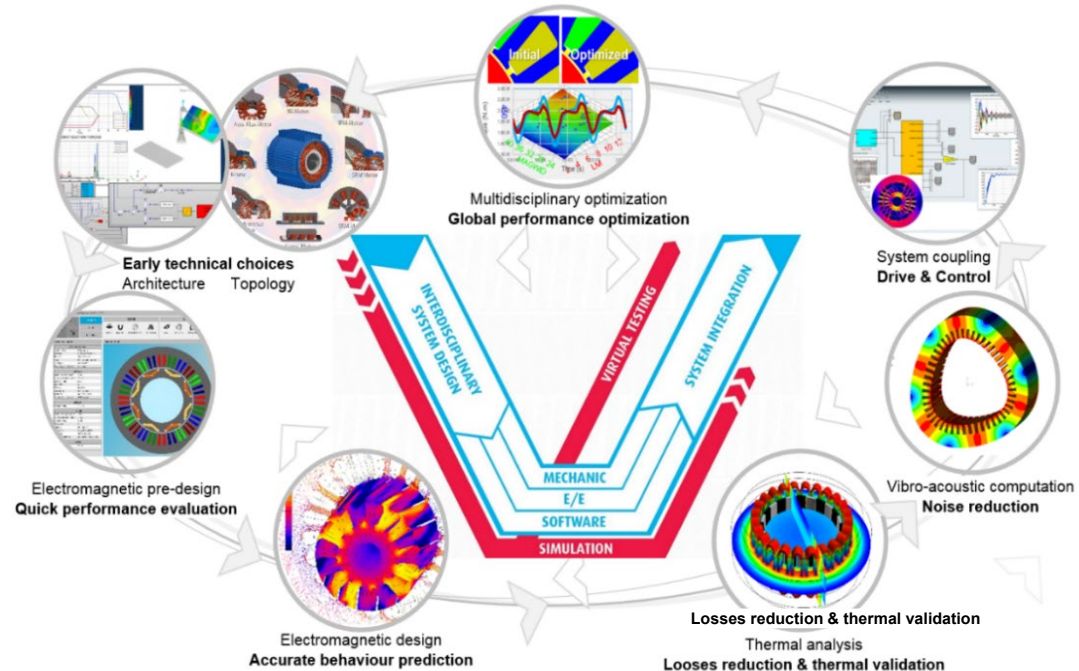


THE E-MOTOR DESIGN PROCESS

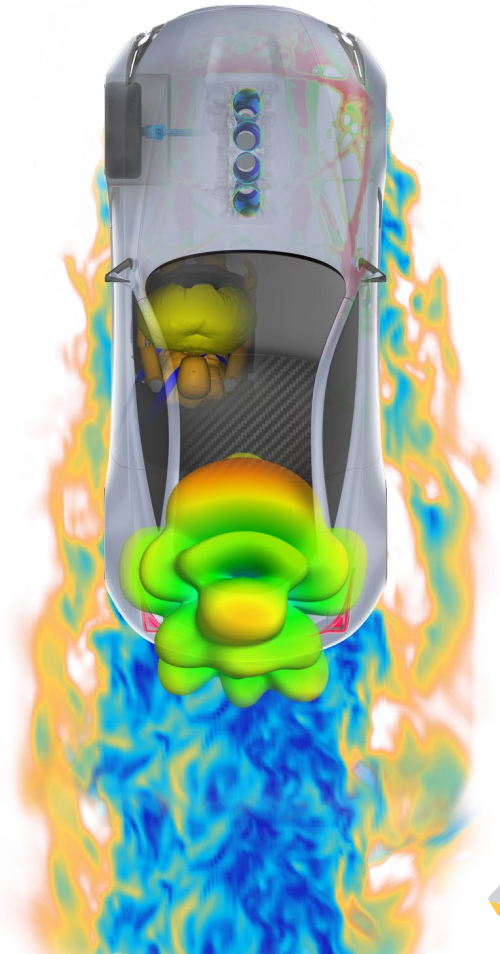
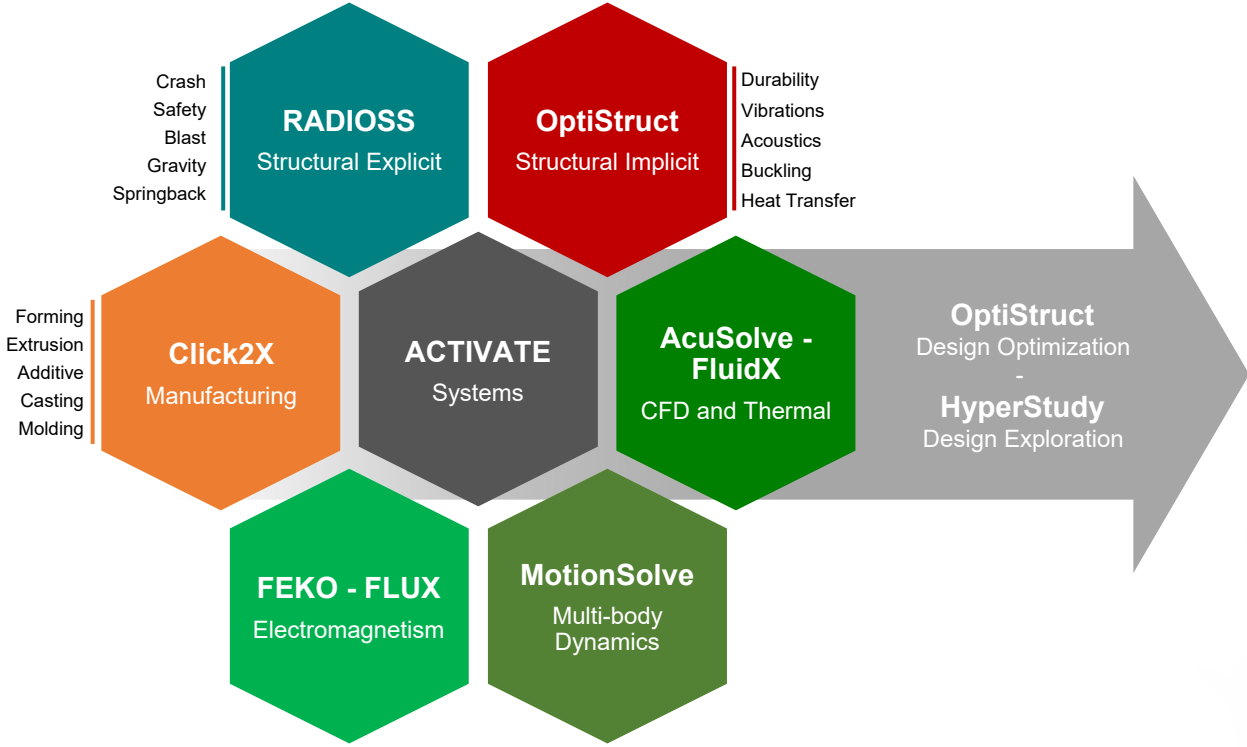


ALTAIR'S COMPLETE PLATFORM FOR E-MOTOR INNOVATION

- An **integrated** workflow for **model based multi-physics optimization** design
- **Disruptive** to traditional design process through **machine learning**
- **Speed to market** with **balanced design** and confidence
- **Flexible process** for customization and ease of use



ALTAIR SOLVER TECHNOLOGY



E-MOTOR DESIGN PROCESS

Philippe W.



DESIGN SPECIFICATIONS

Specifications

- Stator diameter : DIAM
- Active length : LENGTH
- Iron fill factor : 0.92
- Magnet : Br 1.15 T
- Tmax winding : 200°C
- Tmax rotor : 180°C
- Maximum speed : MAXS rpm
- Minimum power : 170kW
- Max phase voltage : 241V
- Max phase current : 300A
- DC-link voltage : 650V, 800V

Objectives

- Maximum power (base point)
- Minimize torque ripple

Constraints

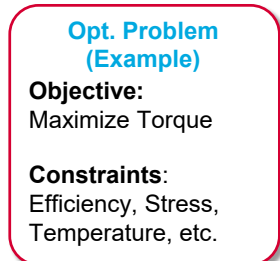
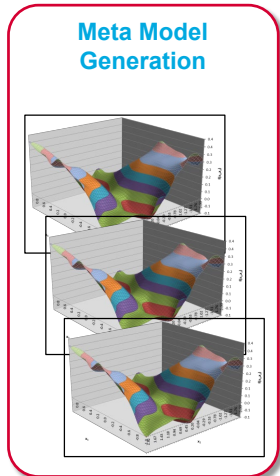
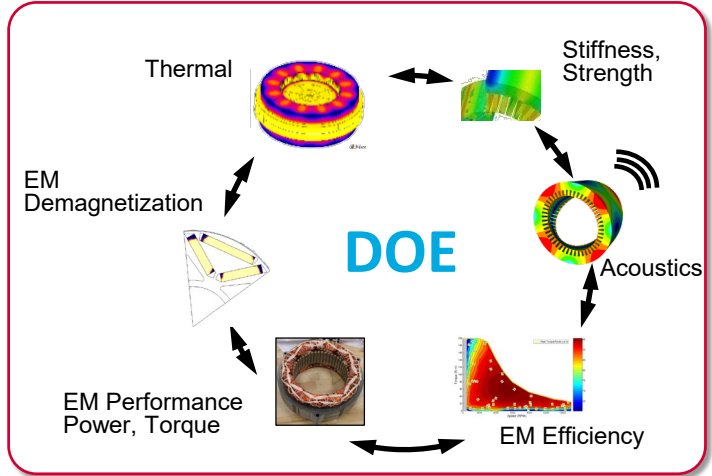
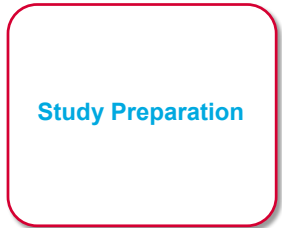
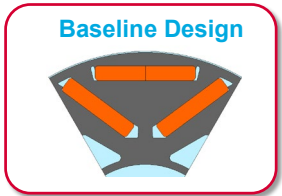
- Demagnetization at base point
- Mechanical strength
- Temperature of winding lower than 200°C

The stator topology is set.

The rotor topology is open



MULTI-DISCIPLINARY/PHYSICS OPTIMIZATION – GENERIC OVERVIEW



Preprocessing

Execute DOE

Postprocessing

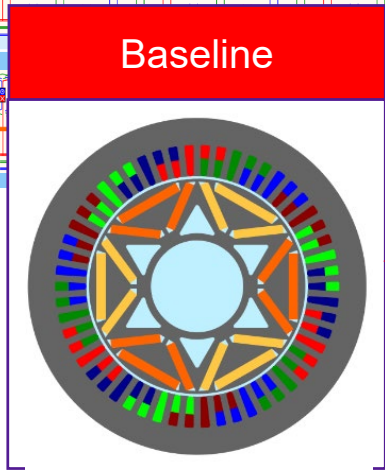
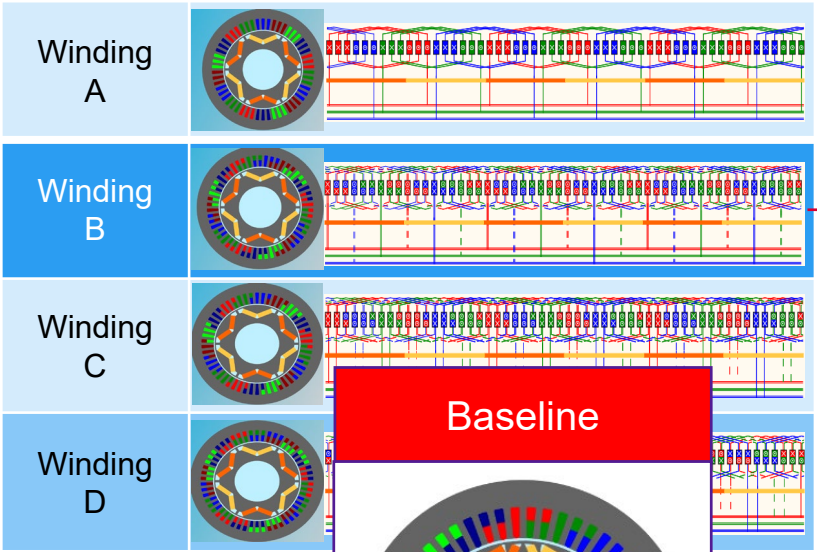


FLUXMOTOR PROJECT BASE DESIGN



MOTOR BASELINE

Winding Selection



Rotor Selection

| | Rotor A | Rotor B | Rotor C | Rotor D |
|----------------------------------|---------|---------|---------|---------|
| | | | | |
| Current den (A/mm ²) | 31,1 | 31,1 | 31,1 | 31,1 |
| Torque (Nm) | 181 | 164 | 165 | 162 |
| Power (kW) | 195 | 186 | 185 | 180 |
| Base speed (rpm) | 10.290 | 10.830 | 10.670 | 10.610 |
| Efficiency (%) | 96,0 | 95,9 | 95,9 | 95,7 |
| Magnet weight (Kg) | 2,54 | 2,48 | 2,48 | 2,53 |



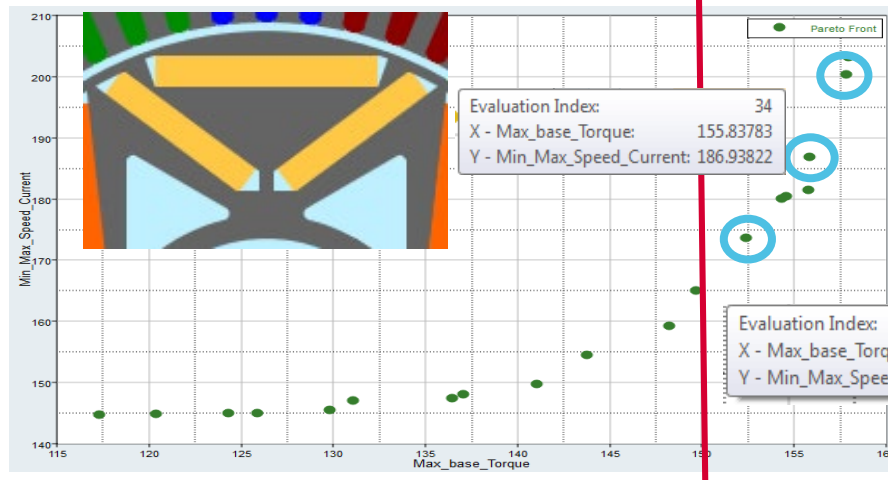
FIRST OPTIMIZATION FLUXMOTOR: MINIMIZE CURRENT

Goal:

- Maximize base torque – more than 150 N.m
- Minimize current at 100 kW (initial value 205 A)

50 runs

30 minutes



With 174 A, we obtain the target torque, helping the temperature constraints



DOE WORKFLOW



LOAD CASES

Base point

- Identify base point
- Average torque and torque ripple
- Short-circuit test, risk for demagnetization

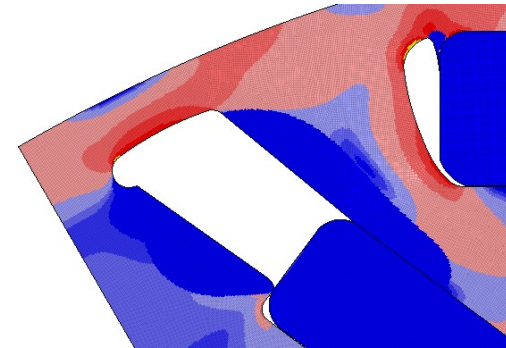
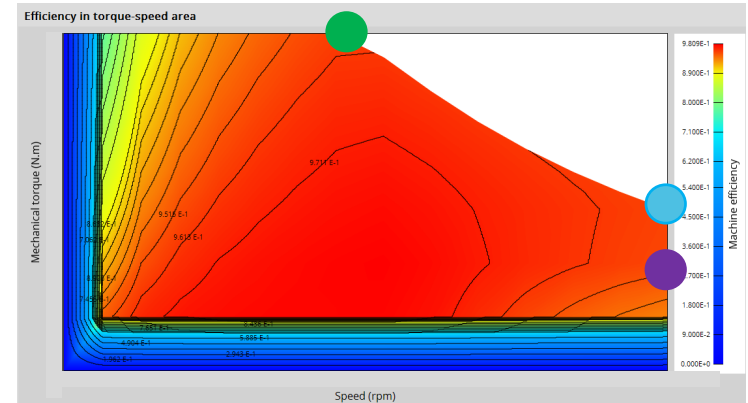
Max speed max torque

- Average torque and torque ripple, losses

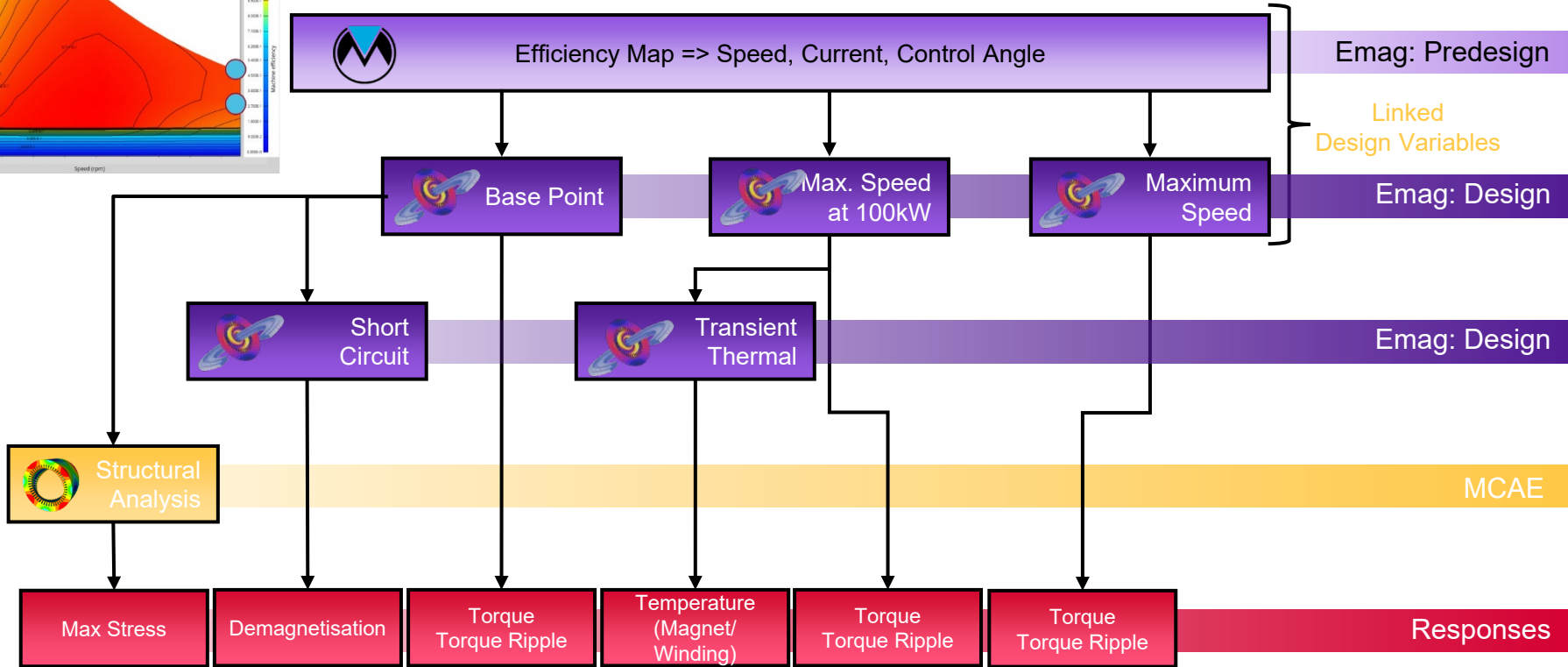
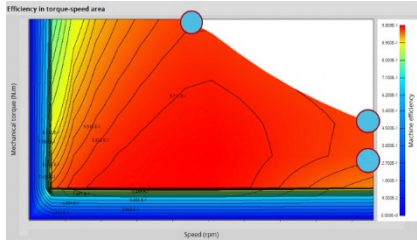
Max speed 100 kW : check temperature after 2 hours

- Magnetic analysis: losses
- 2D Thermal analysis: temperature after 2 hours

Stress : check stress at MAXS rpm on rotor only



WORFLOW TO COMPUTE ONE SINGLE SAMPLE



SETTING THE LOAD CASES



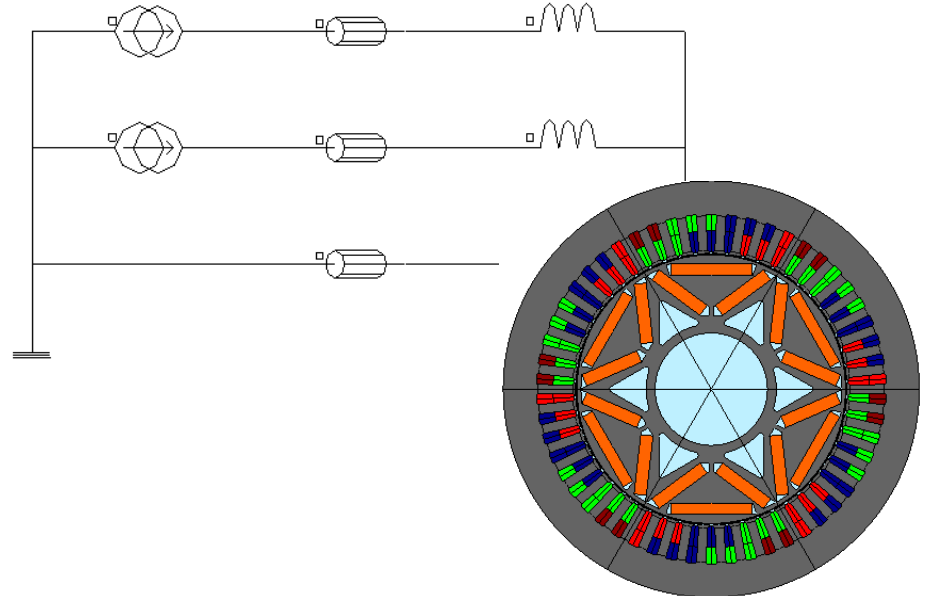
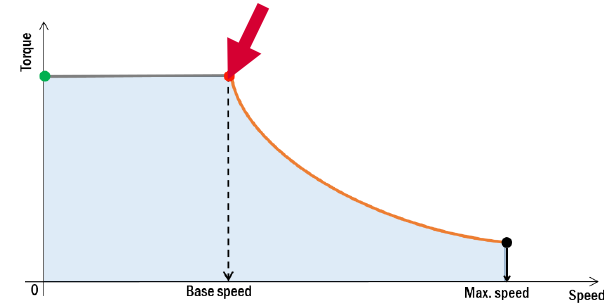
FLUX BASE POINT

Input

- Rotor geometric parameters
- Base speed,
- Base line current,
- Base control angle

Output

- Base torque,
- Base torque ripple,
- Generate *.STEP file (for OptiStruct analysis)



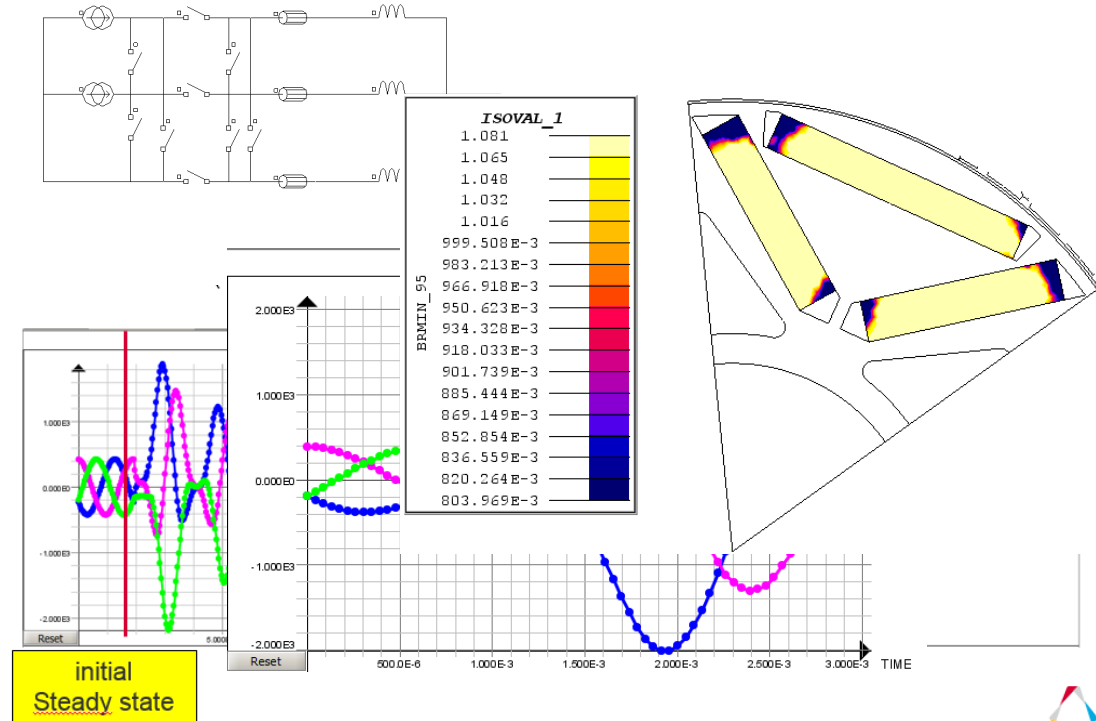
FLUX SHORT-CIRCUIT AT BASE SPEED

Input

- Rotor geometric parameters
- Speed
- Base line current,
- Base control angle

Output

- Demagnetization



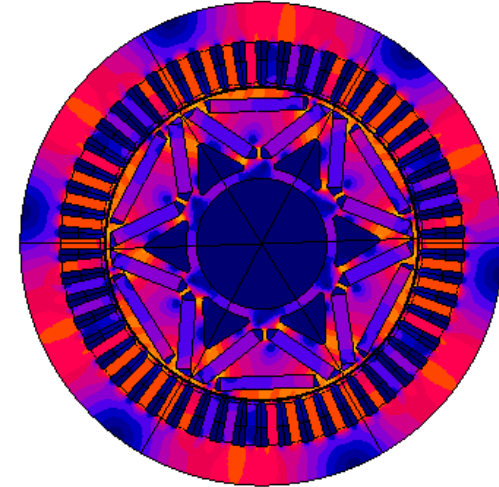
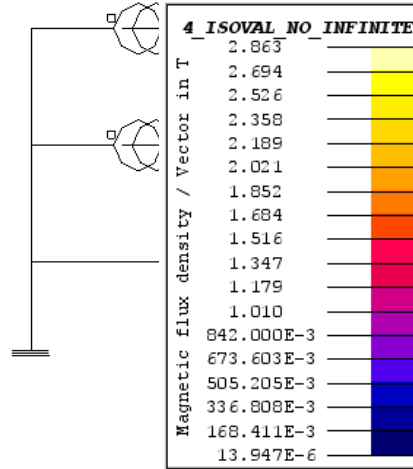
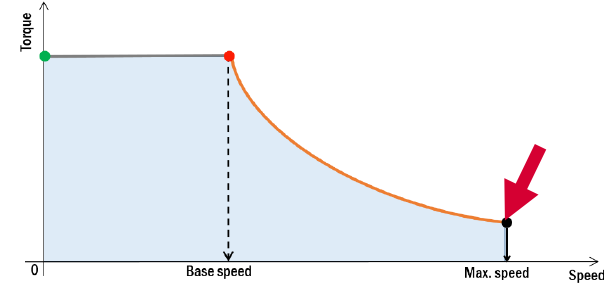
FLUX MAX SPEED

Input

- Rotor geometric parameters
- Speed
- Max speed line current
- Max speed control angle

Output

- Max speed torque
- Max speed ripples



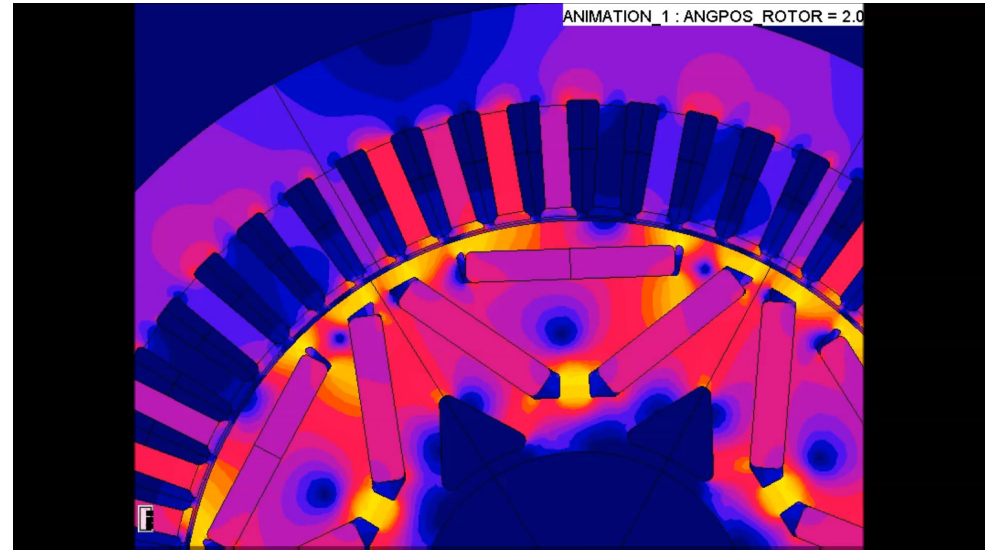
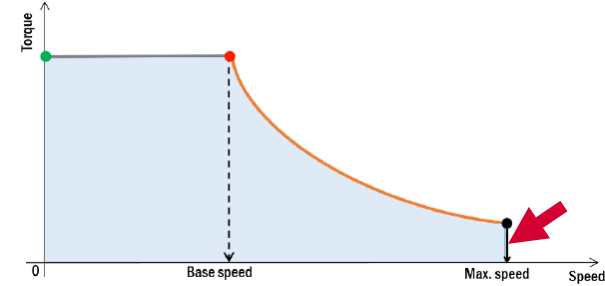
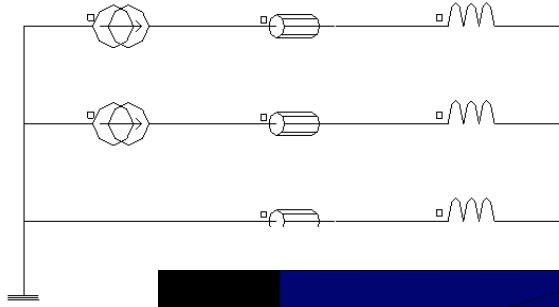
FLUX 100KW AT MAX SPEED

Input

- Rotor geometric parameters
- Speed, current, angle

Output

- Losses (core losses rotor and stator, winding Joule losses, eddy current magnet)



Iron losses



2D THERMAL ANALYSIS

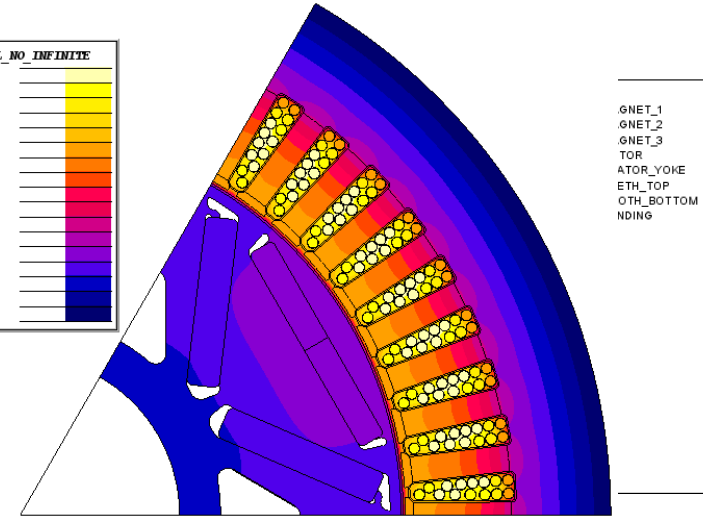
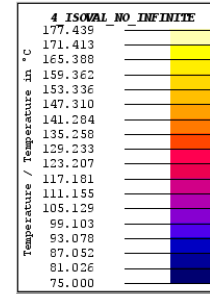
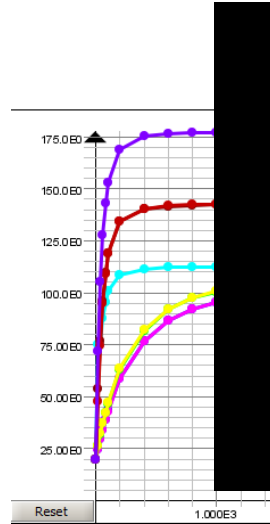
Test after 2 hours

Input :

- Rotor geometric parameters
- Losses

Output

- Temperature in magnets (max)
- Temperature in winding ($T < 180^{\circ}\text{C}$)



STRESS ANALYSIS MAXS

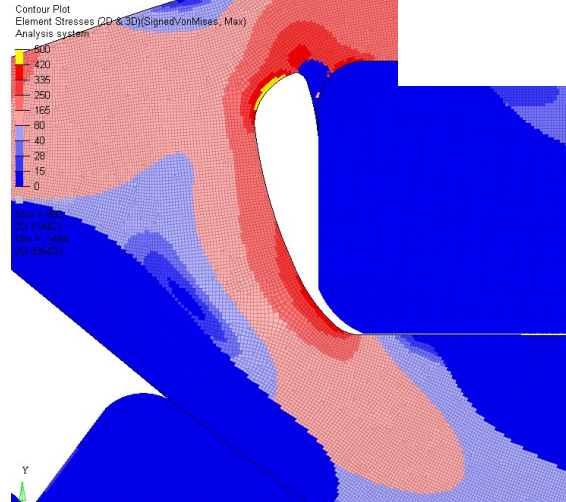
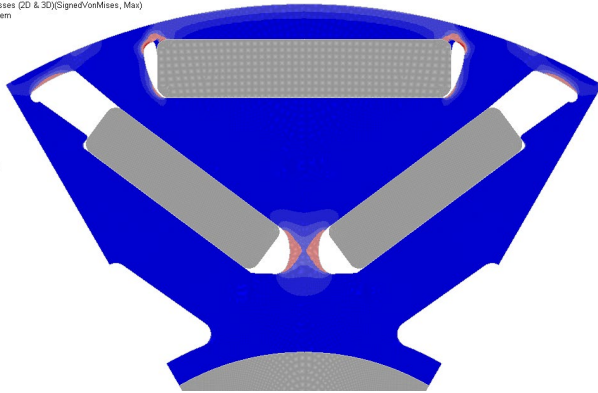
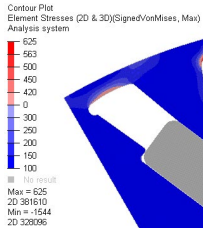
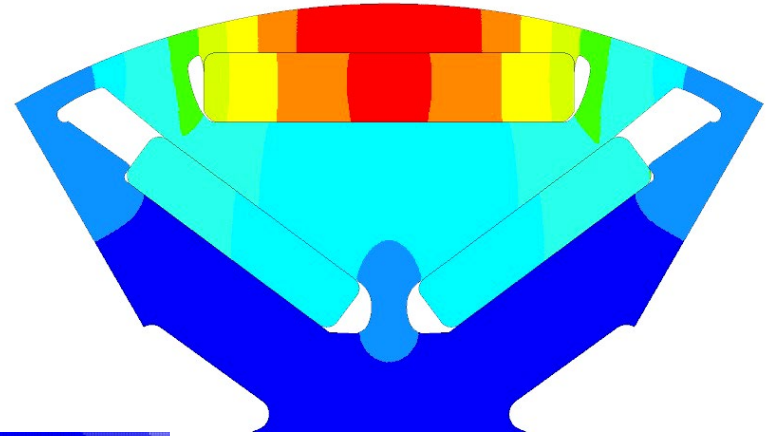
Starting from geometry in step file

Input

- STEP file

Output

- Max value of stress (must be lower than 500 MPa)



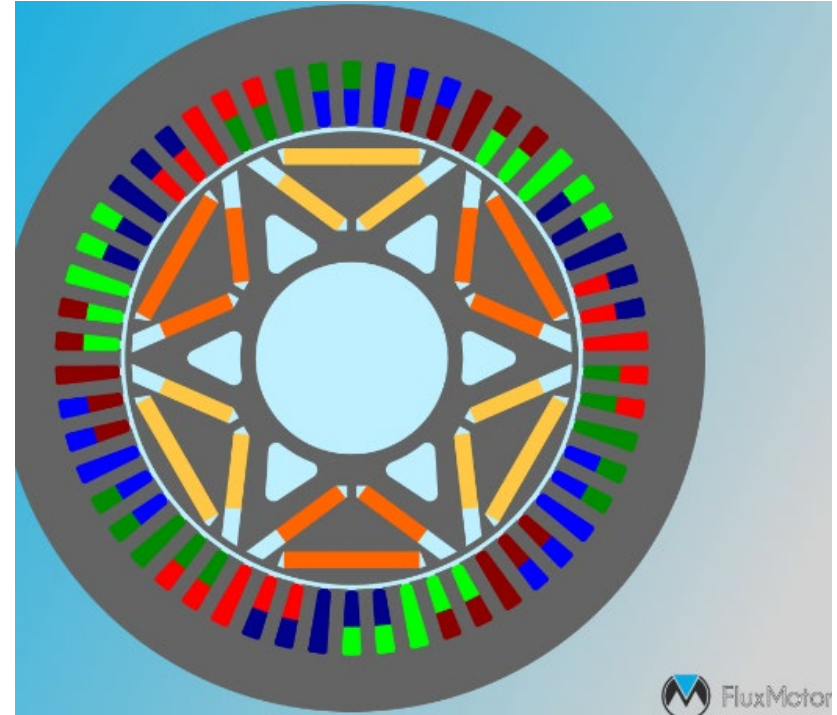
GLOBAL OPTIMIZATION

Goal:

- Maximize base torque
- Minimize torque ripple

Constraint:

- Stress lower than 500 MPa
- Winding temperature lower than 180°C
- Demagnetization lower than 5%
- Torque greater than 150 Nm



DOE OUTLINE

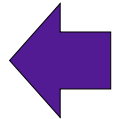
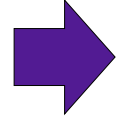
Summary of Optimization Problem in HyperStudy

| + Add Model x Remove Model Model Resources | | | | Solving time | |
|--|-------------------------------------|-----------------|---------|--------------|-------------|
| | Active | Label | Varname | Model Type | |
| 1 | <input checked="" type="checkbox"/> | FluxMotor | m_1 | FluxMotor | 2,5 minutes |
| 2 | <input checked="" type="checkbox"/> | base_speed | m_2 | Flux | 4 minutes |
| 3 | <input checked="" type="checkbox"/> | Max_Speed | m_3 | Flux | 4 minutes |
| 4 | <input checked="" type="checkbox"/> | Short_circuit | m_4 | Flux | 6 minutes |
| 5 | <input checked="" type="checkbox"/> | 100_kW_Max_S... | m_5 | Flux | 4 minutes |
| 6 | <input checked="" type="checkbox"/> | Thermal | m_6 | Flux | 6 minutes |
| 7 | <input checked="" type="checkbox"/> | HyperMesh | m_7 | Operator | 10 seconds |
| 8 | <input checked="" type="checkbox"/> | OptiStruct | m_8 | Operator | 2 minutes |

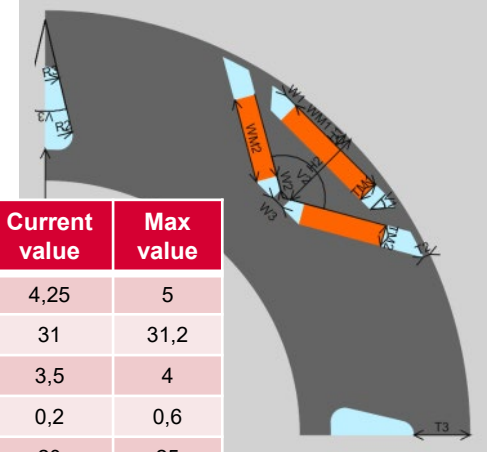
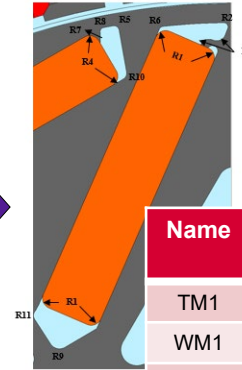
29 minutes

DOE Study

- 18 Design Variables
- Approximately 400 runs
- 18h with 15 cores in parallel



Design Space



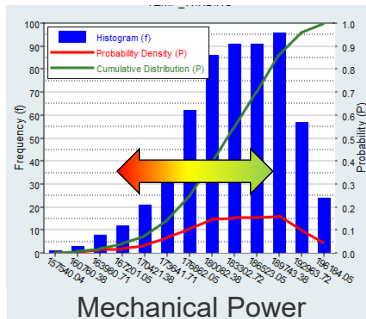
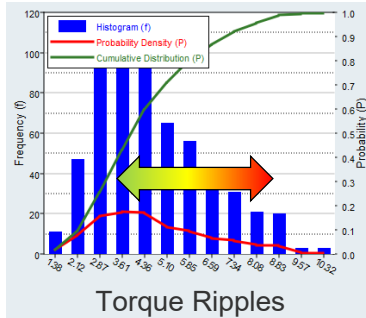
| Name | Min Value | Current value | Max value |
|------|-----------|---------------|-----------|
| TM1 | 3 | 4,25 | 5 |
| WM1 | 29 | 31 | 31,2 |
| H1 | 3 | 3,5 | 4 |
| W1 | 0,2 | 0,2 | 0,6 |
| V1 | 15 | 20 | 25 |
| TM2 | 3,5 | 4,75 | 4,75 |
| WM2 | 16 | 23 | 23 |
| H2 | 20 | 20 | 20 |
| W2 | 0,5 | 0,6 | 0,7 |
| T2 | 1,1 | 1,5 | 1,6 |
| V2 | 106,7 | 107 | 107,1 |



GLOBAL OPTIMIZATION

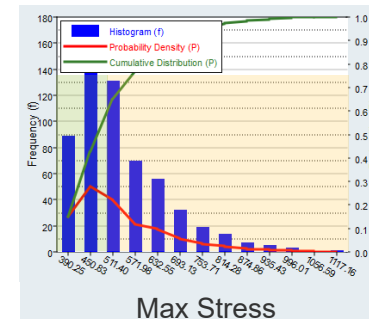
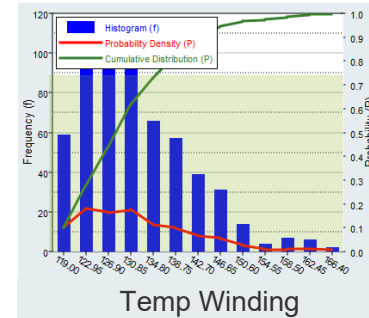
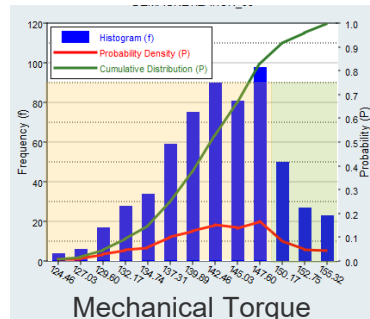
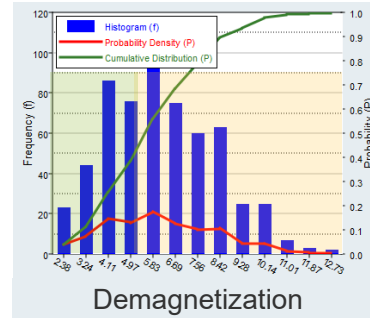
2 Objectives

- Min Torque Ripples
- Max Power

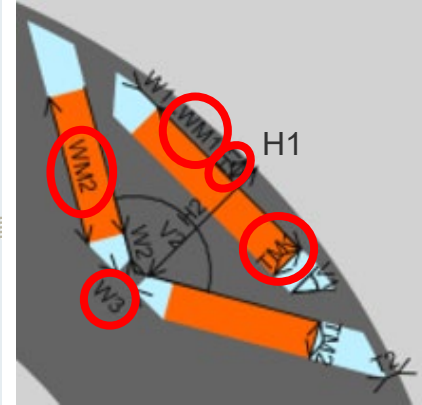
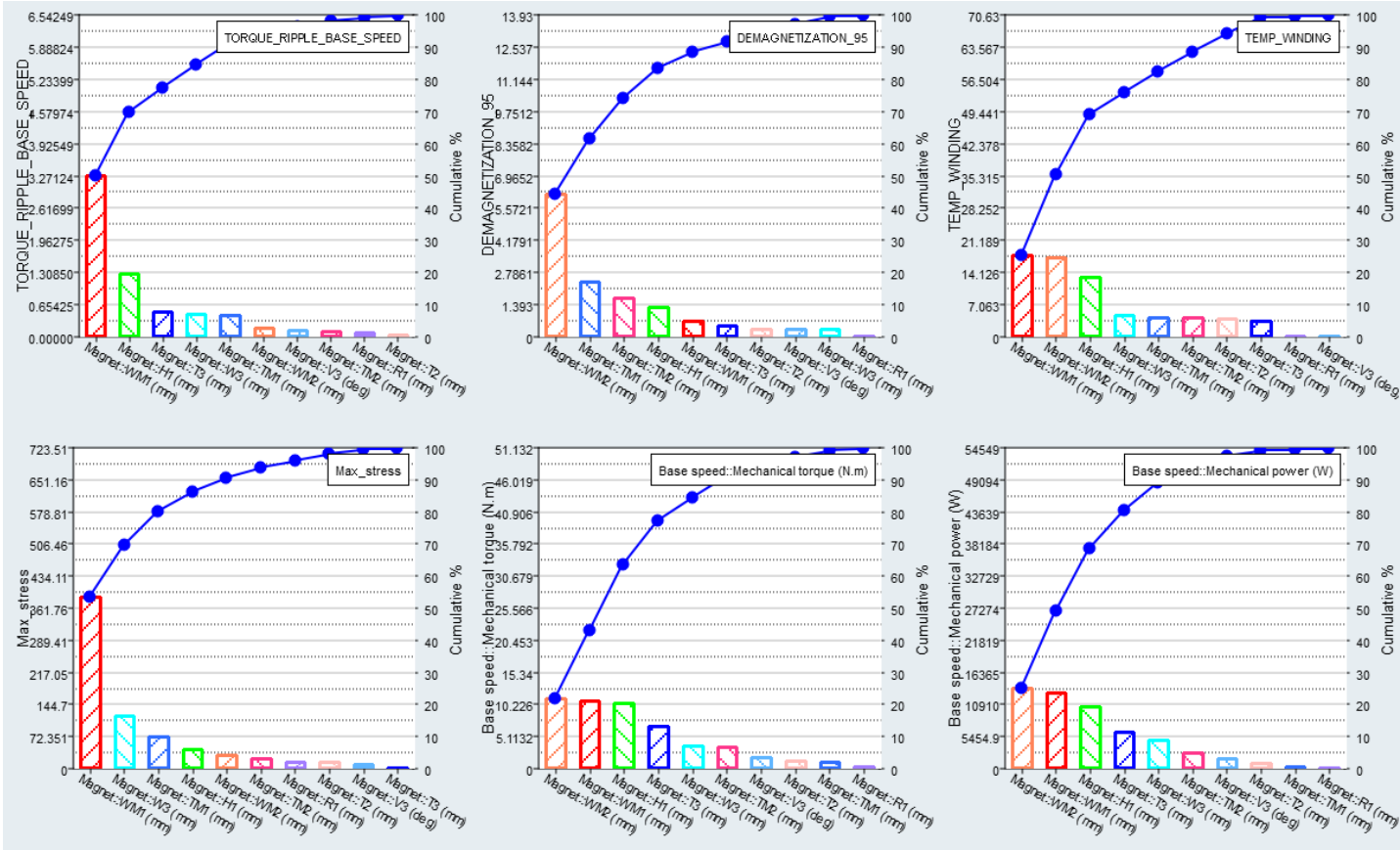


4 Constraints

- Demagnetization < 5 %
- Base torque >= 150 Nm
- Temperature winding < 180°C
- Max stress <= 500 Mpa

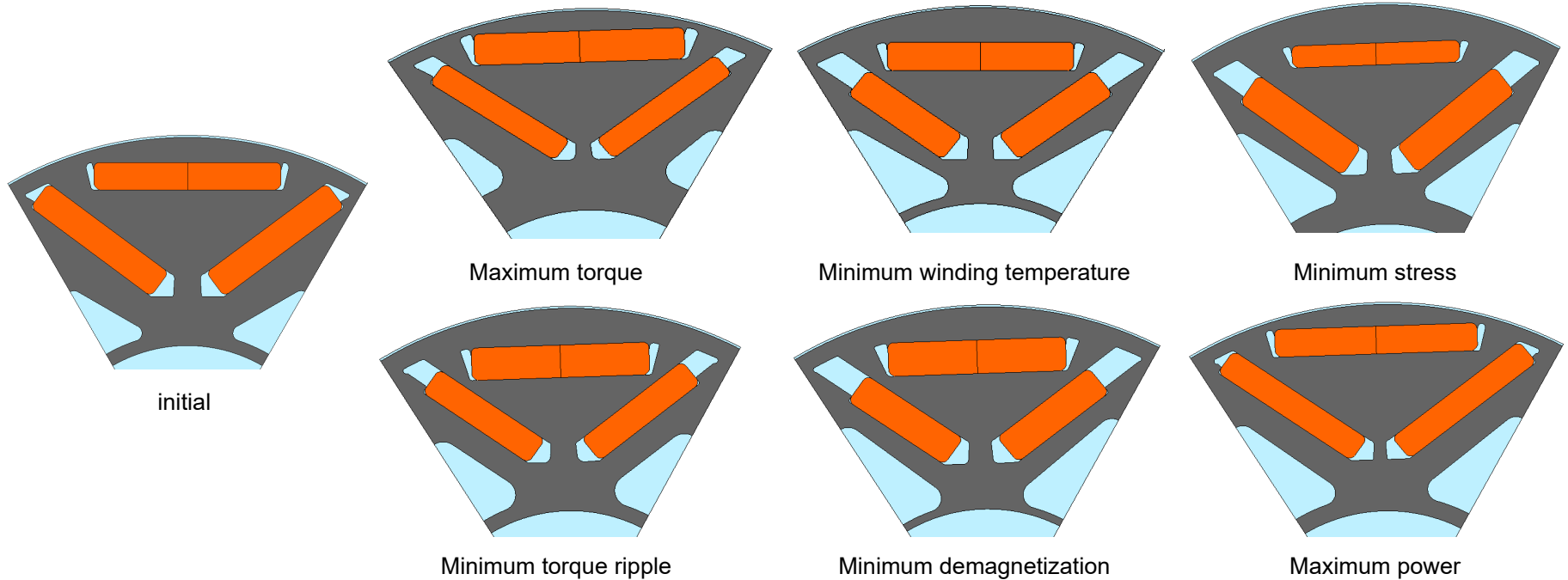


400 RUNS – SENSITIVITY



GLOBAL OPTIMIZATION : DESIGN OF EXPERIMENT

Trends from DOE



OPTIMIZATION



USING FIT FOR DIFFERENT OPTIMIZATIONS

2 objectives

- Max power
- Min torque ripple

• 4 constraints

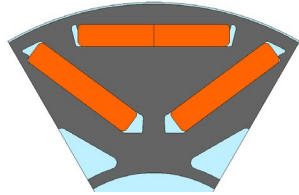
- Max stress ≤ 500 MPa
- Demagnetization ≤ 5 %
- Temperature winding $< 180^\circ\text{C}$
- Base torque $\Rightarrow 150$ Nm

| 500 iterations 12 points per iteration | | | | | | | | | | | |
|--|--------|-----------|--------|----------|-------------|-------------|------------------|------------------|-----------|------------------|--|
| DEMAG | stress | T_winding | Torque | | Objective 1 | Objective 2 | STRESS | DEMAG | WINDING | TORQUE | |
| 5 | 500 | 180 | 145 | optimal | 185558.05 | 3.3028670 | 500.11439 | 5.0013581 | 130.90805 | 144.89983 | |
| 5 | 500 | 180 | 150 | violated | 185508.19 | 3.6410141 | 507.49310 | 5.0686687 | 129.17836 | 144.97804 | |
| 5 | 550 | 180 | 150 | violated | 187568.45 | 3.0975566 | 558.08334 | 5.0524471 | 135.21758 | 146.80096 | |
| 5 | 600 | 180 | 150 | violated | 187670.12 | 4.5006536 | 603.67138 | 5.0290165 | 134.09146 | 148.13142 | |
| 5 | 650 | 180 | 150 | optimal | 189735.28 | 4.3846638 | 651.65516 | 5.0097176 | 137.21773 | 149.29942 | |
| 6 | 500 | 180 | 150 | violated | 187886.74 | 3.6127883 | 504.44520 | 6.0462309 | 132.34385 | 147.29856 | |
| 7 | 500 | 180 | 150 | violated | 189568.45 | 4.0627783 | 502.64007 | 7.0298307 | 134.11429 | 148.39414 | |
| 7,5 | 500 | 180 | 150 | optimal | 190711.88 | 3.3218627 | 499.97401 | 7.4943515 | 136.39664 | 150.02709 | |
| 7,2 | 500 | 180 | 150 | optimal | 190256.56 | 3.4551889 | 500.39643 | 7.2047921 | 135.50755 | 149.77043 | |

Note: with fit, one optimization takes less than 2 minutes with 500 runs



E-MOTOR OPTIMIZATION PROBLEM – FINAL RESULTS



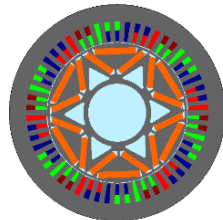
• Optimization Objective:

- Maximize base output Power
- Minimize base Torque Ripple

• Constraints:

- Stress lower than 500 MPa
- Winding Temperature lower than 180°C
- Demagnetization lower than 5%
- Base Torque greater than 150 Nm

| | Initial |
|-------------------------|---------|
| Base torque [Nm] | 155 |
| Base torque Ripple [Nm] | 8,5 |
| Stress [Mpa] | 2.316 |
| Winding Temp. [°C] | 171 |
| Demagnetization Factor | 6,6 |



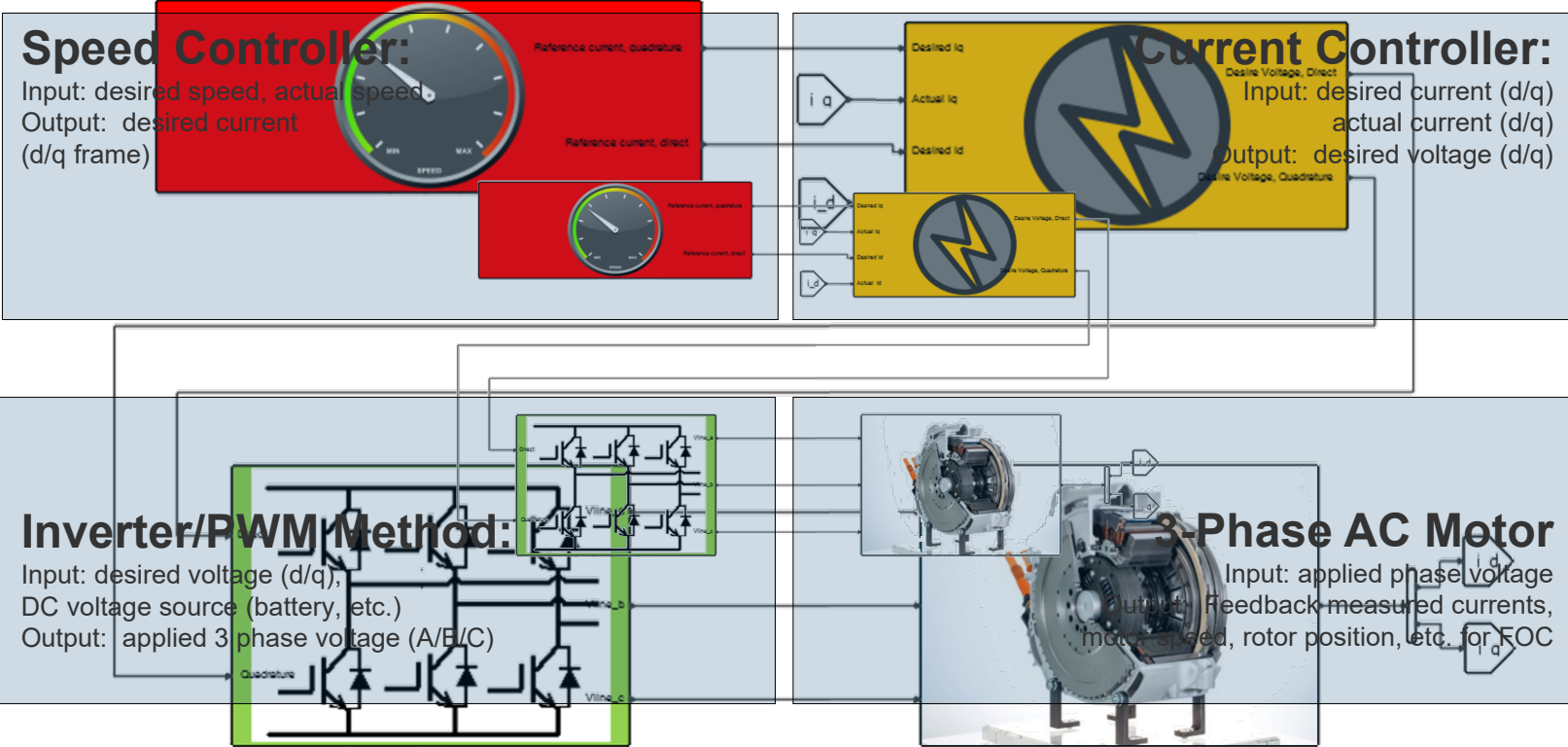
Magnet Weight
Reduction of 40 %



TO GO FURTHER: INCLUDE DRIVE

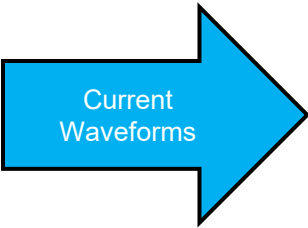
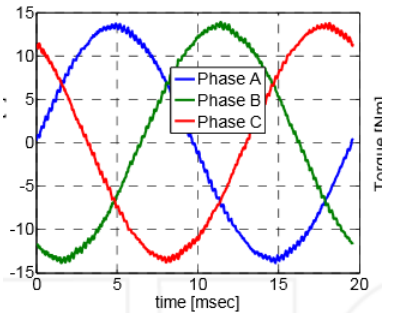
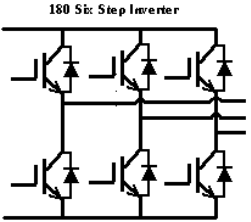
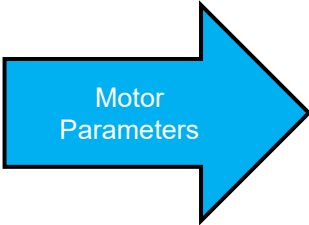


FIELD ORIENTED CONTROL STEPS: OVERVIEW

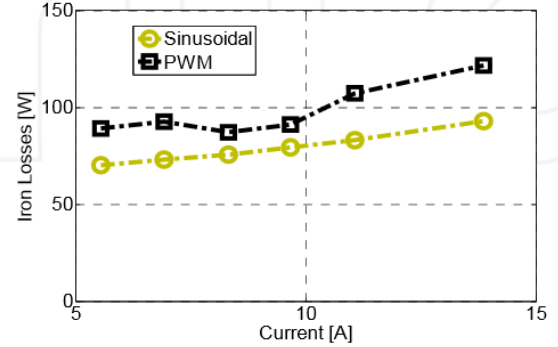
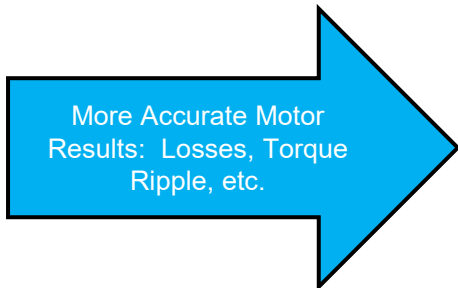


PROCESS: ACTIVATE INVERTER INPUTS TO FLUX

Flux



Flux

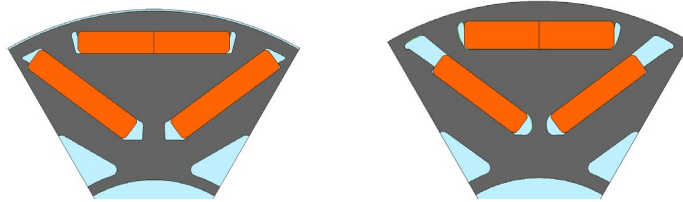


*Image Source: <https://cdn.intechopen.com/pdfs-wm/39370.pdf>
See notes, next slide for details

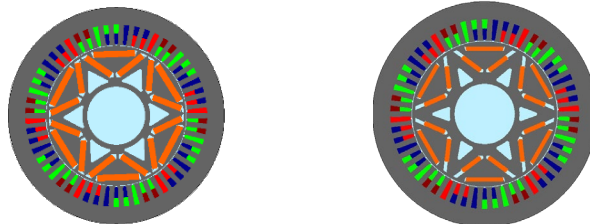
Faster process than direct co-sim:
Use simplified motor model in Activate to generate steady-state current



E-MOTOR OPTIMIZATION PROBLEM – FINAL RESULTS WITH PWM



| | Initial | Current Optimum With Sine Current |
|-------------------------|---------|--------------------------------------|
| Base torque [Nm] | 155 | 150 |
| Base torque Ripple [Nm] | 8,5 | 5,4 |
| Stress [Mpa] | 2.316 | 500 |
| Winding Temp. [°C] | 171 | 139 |
| Demagnetization Factor | 6,6 | 5,2 |

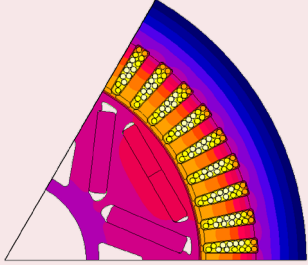
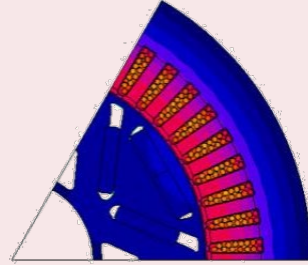
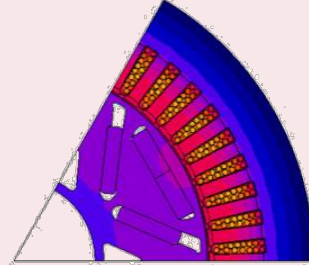
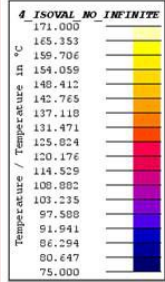


Magnet Weight
Reduction of 40 %



(*) TEMPERATURES USING PWM CURRENT

| | Initial | Current Optimum With Sine Current | Current Optimum with PWM Current (620V – 800V) |
|------------------------|----------|-----------------------------------|--|
| Joule losses (W) | 4.220 | 2.266 | 2.272 – 2.278 |
| Magnet losses (W) | 143,6 | 58 | 141 - 164 |
| Iron losses stator (W) | 1.157 | 1.096 | 1.173 – 1.206 |
| Iron losses rotor (W) | 230 | 159 | 196 - 208 |
| Temp. Rotor [°C] | Tmax 118 | Tmax 87 | Tmax 103 - 108 |

| | |
|---|------|
|  | High |
|  | |
|  | |
|  | Low |

Added losses leads to 20 % higher temperatures in magnets and rotor yoke



SUMMARY

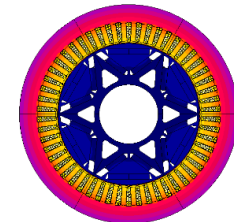
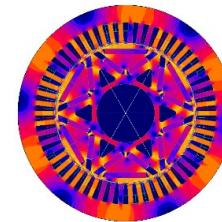
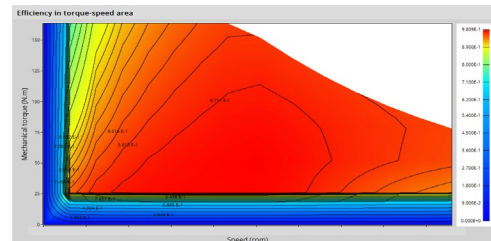
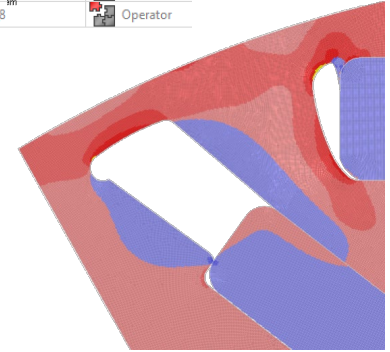
Multi-physics optimization of E-motor including:

- Predesign of motor - FluxMotor
- Magnetic analysis - Flux
- Thermal analysis - Flux
- Structural analysis - OptiStruct

DOE and optimization driven by HyperStudy

Extension system - Activate

| + Add Model | | x Remove Model | | Model Resources | |
|-------------|-------------------------------------|-----------------|---------|-----------------|-----------|
| | Active | Label | Varname | Model Type | |
| 1 | <input checked="" type="checkbox"/> | FluxMotor | m_1 | | FluxMotor |
| 2 | <input checked="" type="checkbox"/> | base_speed | m_2 | | Flux |
| 3 | <input checked="" type="checkbox"/> | Max_Speed | m_3 | | Flux |
| 4 | <input checked="" type="checkbox"/> | Short_circuit | m_4 | | Flux |
| 5 | <input checked="" type="checkbox"/> | 100_kW_MAX_S... | m_5 | | Flux |
| 6 | <input checked="" type="checkbox"/> | Thermal | m_6 | | Flux |
| 7 | <input checked="" type="checkbox"/> | HyperMesh | m_7 | | Operator |
| 8 | <input checked="" type="checkbox"/> | OptiStruct | m_8 | | Operator |

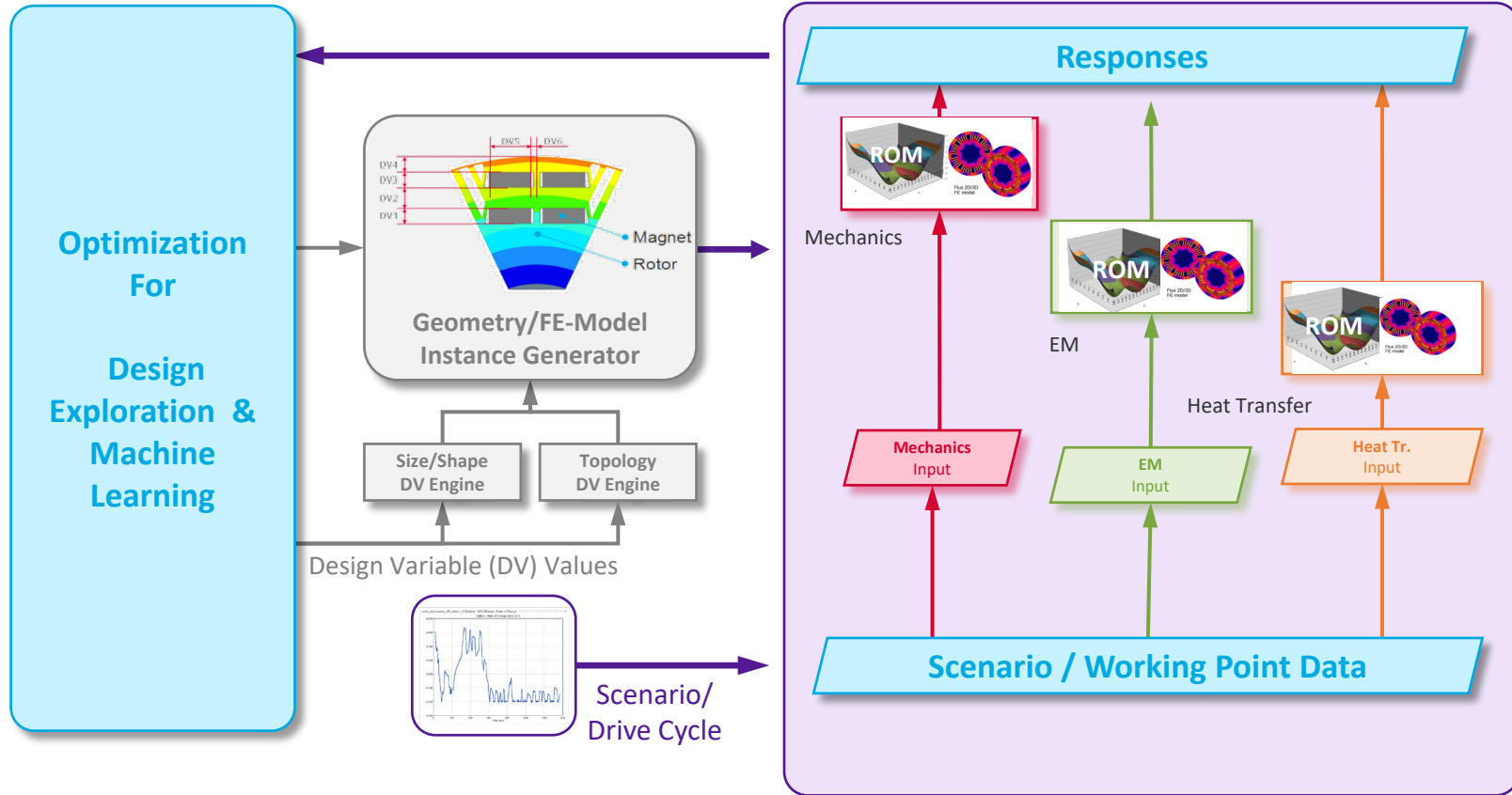


LOOKING FORWARD

Richard Y.



A COMPLETE MODEL BASED MULTIPHYSICS OPTIMIZATION WORKFLOW



EVALUATION OF WLTP – DRIVE CYCLE EFFICIENCY

BEV_v6.scm - Altair Activate Professional Edition 2019.1

Battery Electric Vehicle (BEV) Powertrain Drive Cycle Evaluation

The simulation interface displays the following components and plots:

- Instantaneous Motor Efficiency:** A line graph showing efficiency values between 0.90485 and 0.90500.
- Battery Pack Average State of Charge (SOC):** A line graph showing SOC decreasing from 0.750000 to approximately 0.749994 over time.
- Vehicle Range Scope:** A line graph showing vehicle range in miles, with values between 0.0 and 1.0.
- Vehicle Speed (kph) - Desired Drive Cycle vs. Actual:** A line graph comparing desired (blue) and actual (red) vehicle speeds over 1800 seconds. The y-axis ranges from -0.25 to 0.200 kph.
- E-motor: Torque (N-m) vs. Speed (rpm) in Drive Cycle:** A line graph showing torque (N-m) vs. speed (rpm). The y-axis ranges from -200 to 200 N-m, and the x-axis ranges from 0 to 12000 rpm. Two curves are shown: a blue curve for positive torque and a green curve for negative torque.



Thank you !

For more information about Altair tools, please visit
www.altairhyperworks.com

